

A High Efficiency Inertial CO₂ Extraction System (ICES)

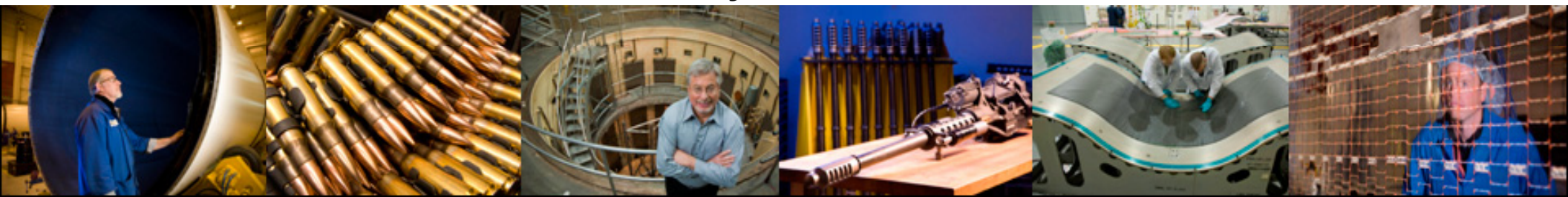
**Dr. Anthony Castrogiovanni, Dr. Vladimir Balepin,
Andrew Robertson, and Bon Calayag**

Presented at the



Advanced Research Projects Agency • ENERGY

**NETL CO₂ Capture Technology Meeting
Pittsburgh, PA
July 11, 2012**



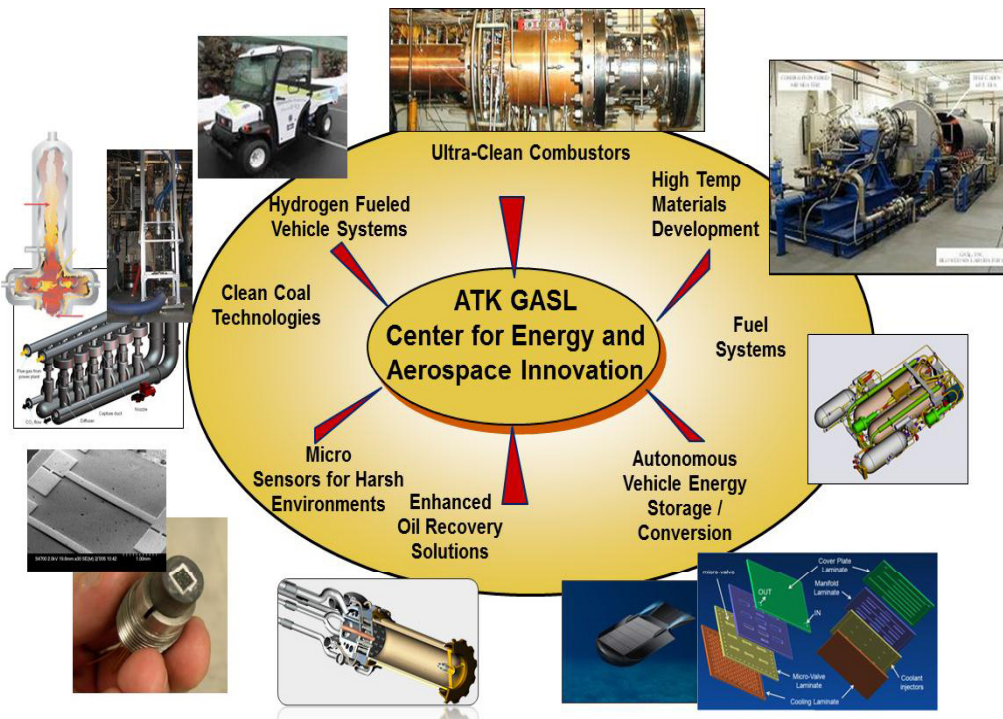
Company Backgrounds



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- ATK is a leading aerospace & defense contractor
- ATK GASL in Ronkonkoma, NY operates the ATK Center for Energy and Aerospace Innovation
- Expertise and research interests include :
 - Aerospace propulsion
 - Carbon capture
 - Hydrogen fueled vehicles
 - Clean coal technologies
 - Oil recovery solutions



- ACENT is a small business dedicated to applying expertise in aerospace and defense to clean energy challenges
- Founded in 2007, ACENT is developing technologies in CO₂ capture, algal biomass, hydrogen vehicles, and enhanced oil recovery



- ICES utilizes some methods developed under a DOE SBIR with ACENT



Funding Summary:

ARPA-e:	\$ 2,693 K
ATK and ACENT Cost Share:	\$ 632 K
NYSERDA (New York State)	<u>\$ 200 K</u>
TOTAL	\$ 3,525 K

Project Performance Dates:

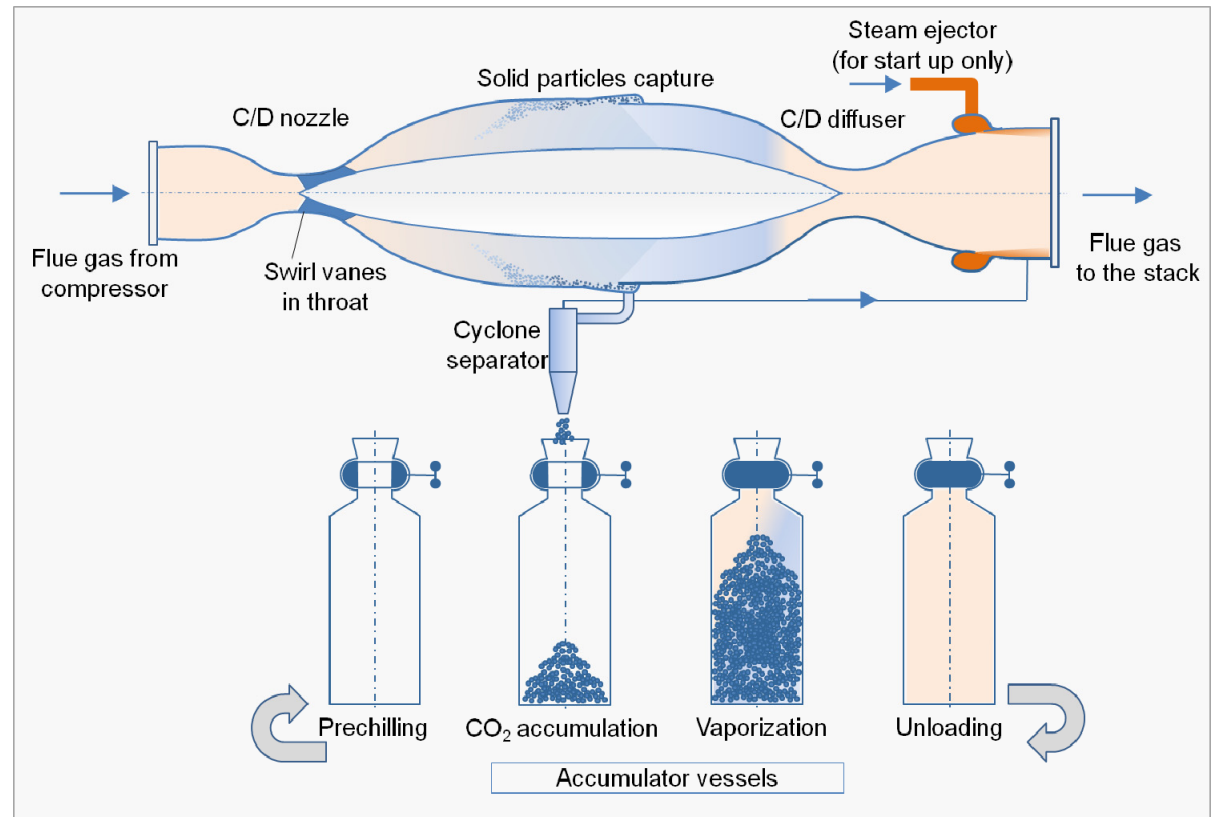
Phase 1:	July 2010 – March 2011 (completed)
Phase 2:	July 2011 – June 2013 (ongoing)

Project Participants:

Alliant Techsystems (ATK)
ACENT Laboratories LLC
WorleyParsons

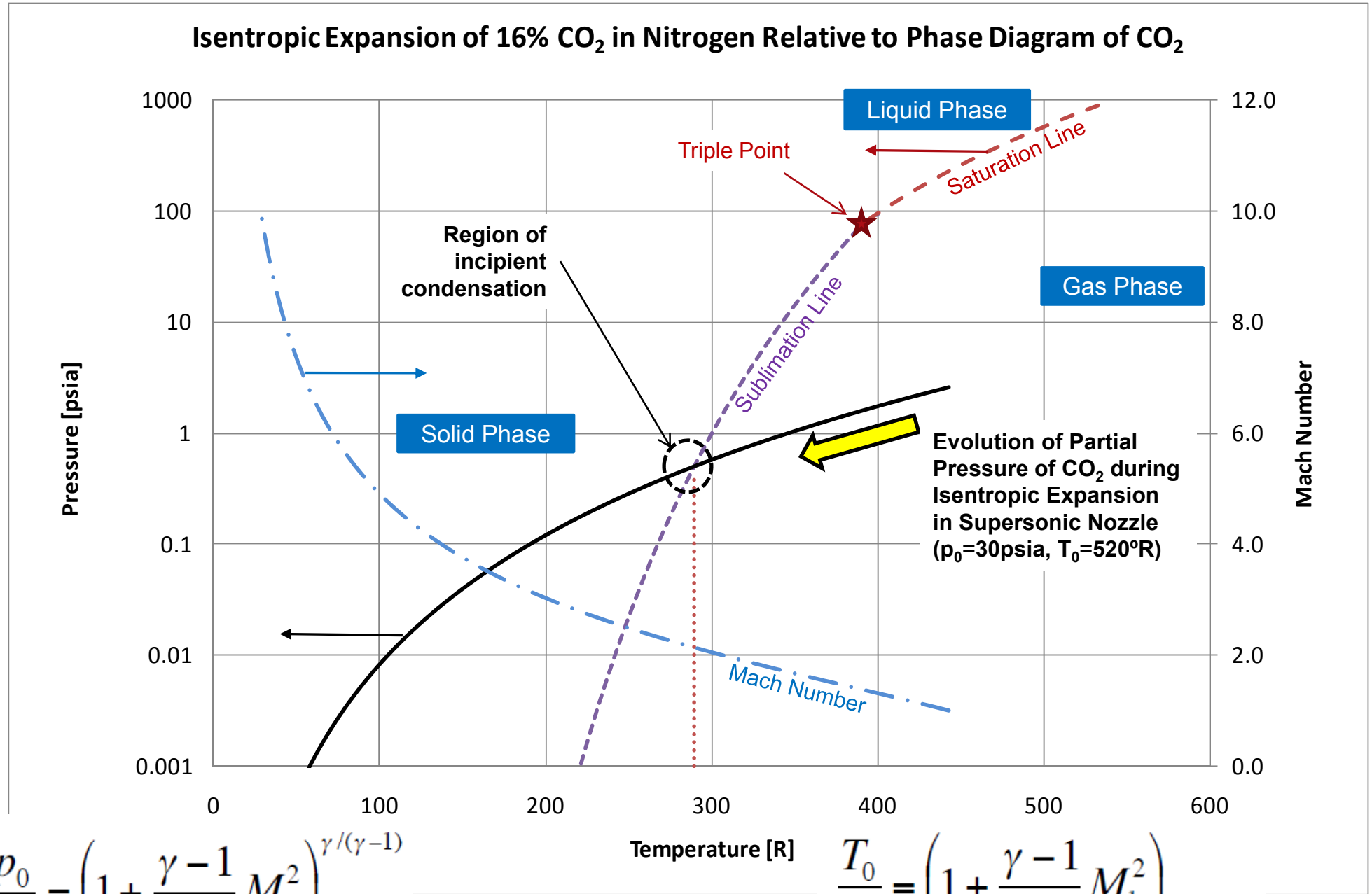
- **Demonstrate proof-of-concept of aero-thermodynamic CO₂ condensation and separation**
- **Develop and benchmark analysis tools with experimental data to enable:**
 - Scaling of demo system to power plant size
 - Projection of economics in terms of COE and parasitic loads
- **Provide basis for next-phase slip-stream testing with real flue gas**
 - Minimize flue gas pressurization requirements
 - Maximize CO₂ capture (>90% goal)

- Pulverized coal power plant flue gas contains ~16% CO₂ in gaseous form at low pressure
- In ICES we compress flue gas to a moderate level and use the low temperature created by supersonic expansion to freeze the CO₂ in the flow
- ICES uses turning induced in the flow to inertially separate the solid particles from the gas stream
- We capture and collect the CO₂ (as dry ice) and then process using a self-pressurization system exploiting power plant waste heat



ICES on a P-T Diagram – Supersonic Expansion

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$$\frac{p_0}{p_1} = \left(1 + \frac{\gamma - 1}{2} M_1^2 \right)^{\gamma / (\gamma - 1)}$$

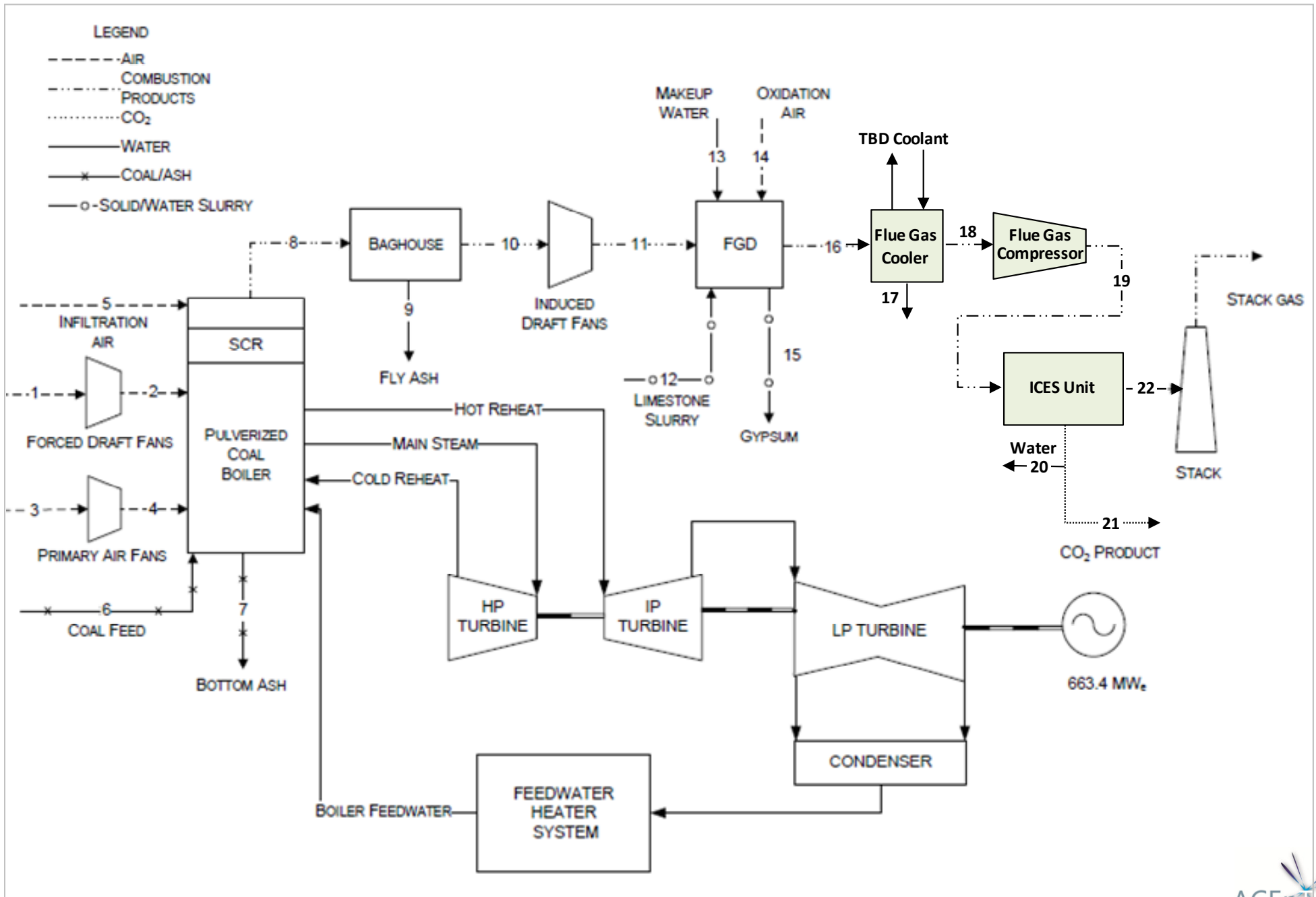
Temperature [R]

$$\frac{T_0}{T_1} = \left(1 + \frac{\gamma - 1}{2} M_1^2 \right)$$

ICES Integration in PC Plant



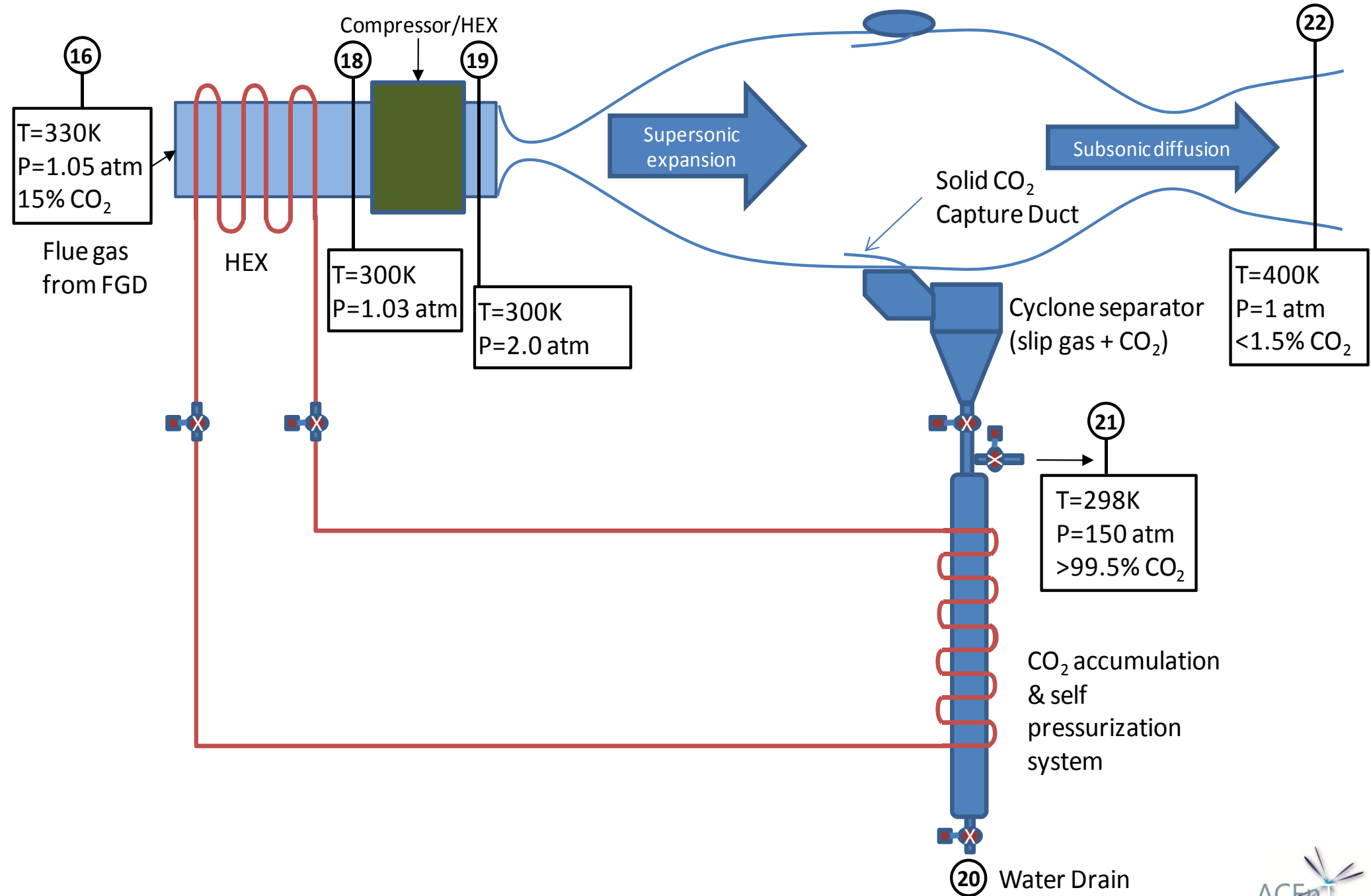
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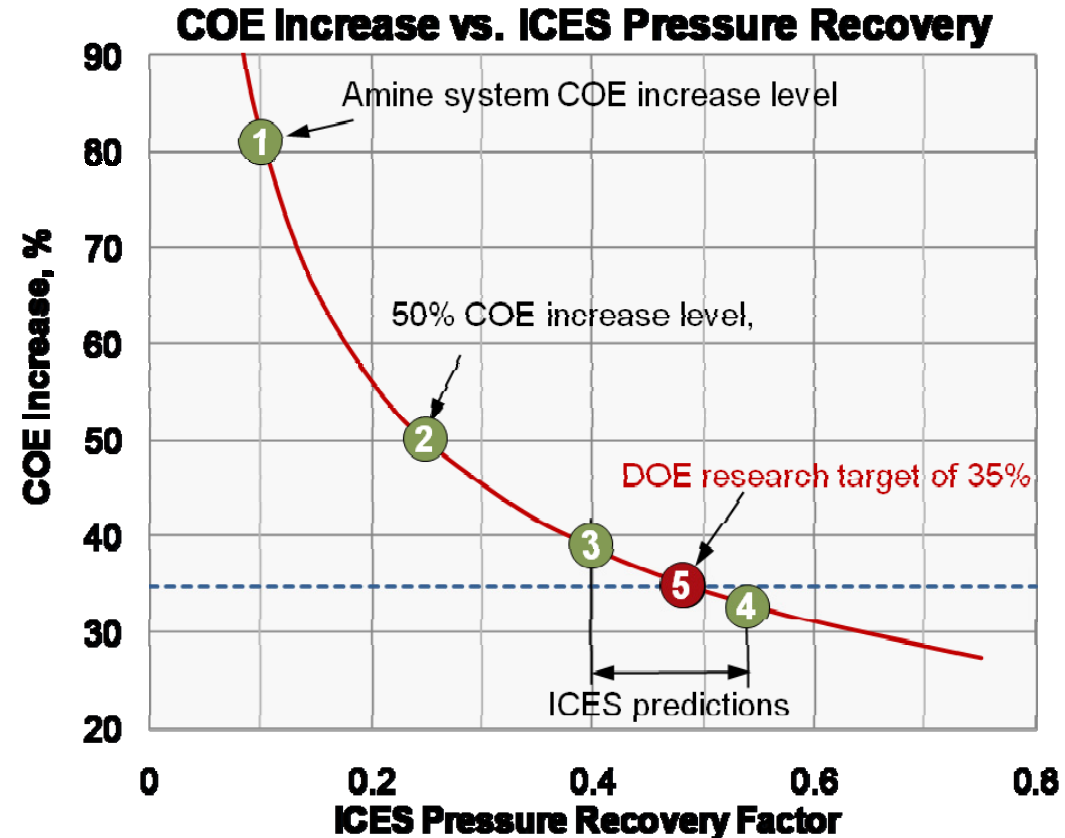
ICES System Schematic



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- ICES operating costs are driven by flue gas pre-compression
- Pressure recovery factor = P_{22}/P_{19}
- Low CapEx/OpEx combined with low power consumption result in a projected cost of electricity increase for CO₂ capture just over 1/3 that of the amine process
- Compression to 2,250 psi from low grade waste heat (constant volume heat addition to solid). Cost is limited to CAPEX + energy to move media.

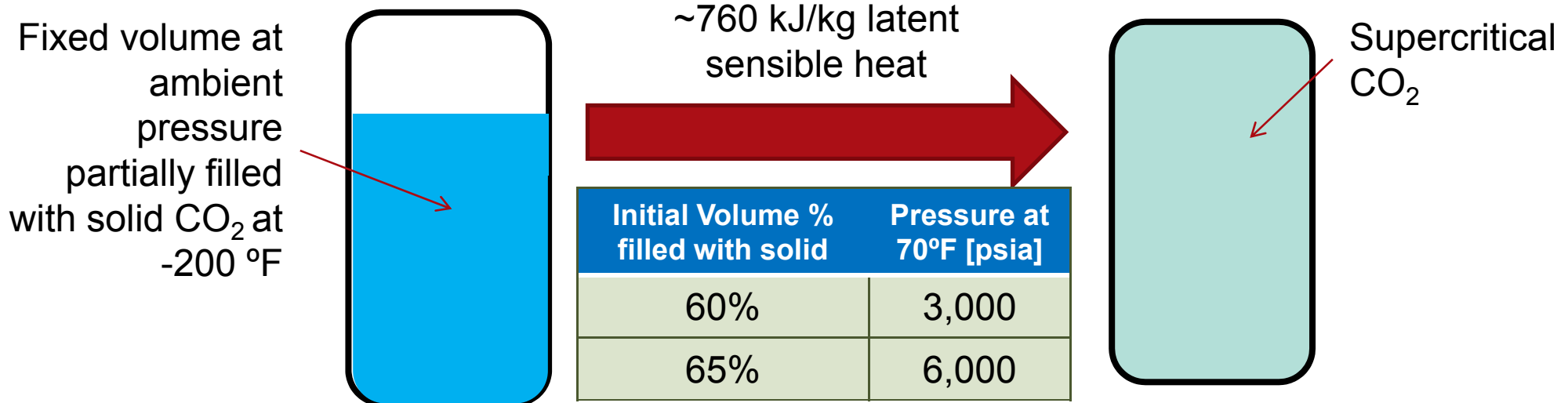


Metric	ICES	Amine
COE % increase	35%	81%
Parasitic Load	12.5%	21.5%
Cost per ton of CO ₂ avoided	US\$ 27	US\$ 68

Process	Minimum Energy [kJ/kg CO ₂]	ICES [kJ/kg CO ₂]	Amine [kJ/kg CO ₂]
Separation	-175	-683*	-
CO ₂ Compression	-247	~68**	-
Total	-422	-751	-1,506

* Pre-compression of flue gas to 2 bar (absolute)

** + Approximately 760 kJ/kg of low grade waste heat used to compress CO₂ from solid phase to 2,250psia



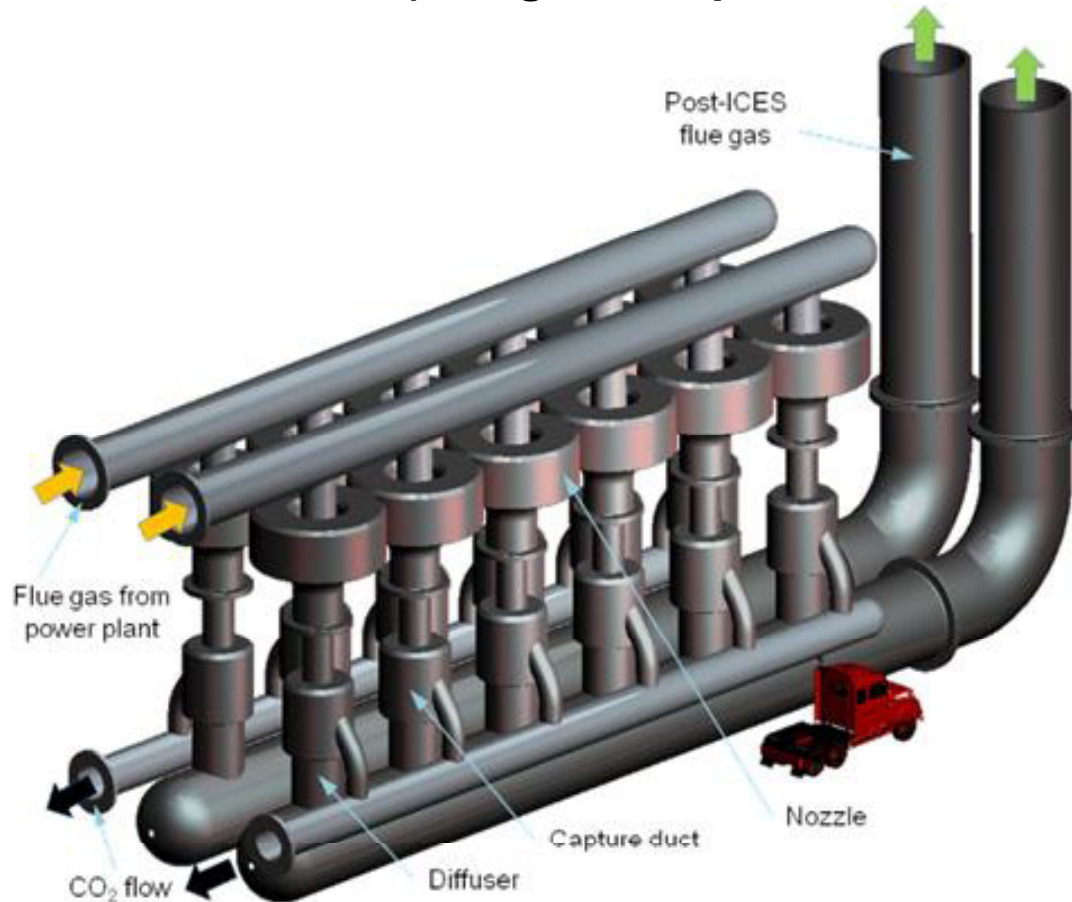
Compression energy is nearly “economically free” but it is not “thermodynamically free” i.e. this energy would otherwise be wasted

ICES Plant Integration and Footprint



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An ICES system sized for 545MW-equivalent flue gas contains twelve 60" ICES units (flue gas compression not shown)



L= 183 ft
W= 60 ft
H = 70ft

ICES is projected to have a significantly smaller footprint and complexity compared to competing CO₂ capture technologies and hence significantly lower capital and maintenance costs

- No moving parts (after start)
- No chemicals/additives or other consumable media
- No refrigeration expense – low temperatures from supersonic expansion
- Inexpensive construction (concrete, sheet metal)
- Small footprint
 - ICES units in test are equivalent to 0.3-0.6 MW slip stream
 - The latest unit (0.3 MW) is 24" x 24" x 3"
- Small size enables distributed deployment for other process applications in the petroleum and chemical industries
- Availability of “cold sink” in solid CO₂ accumulated

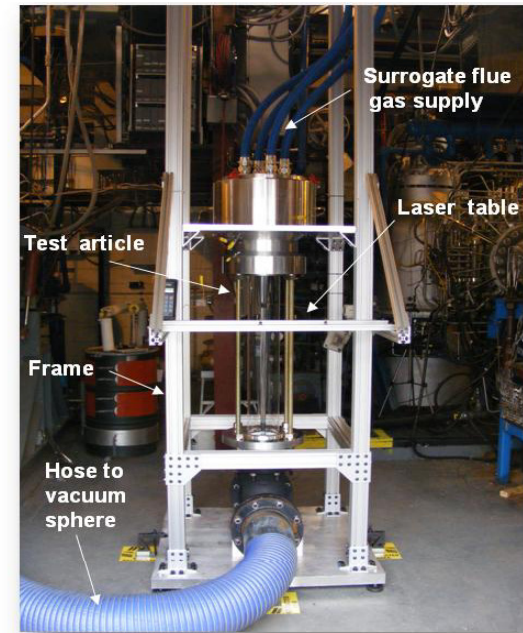
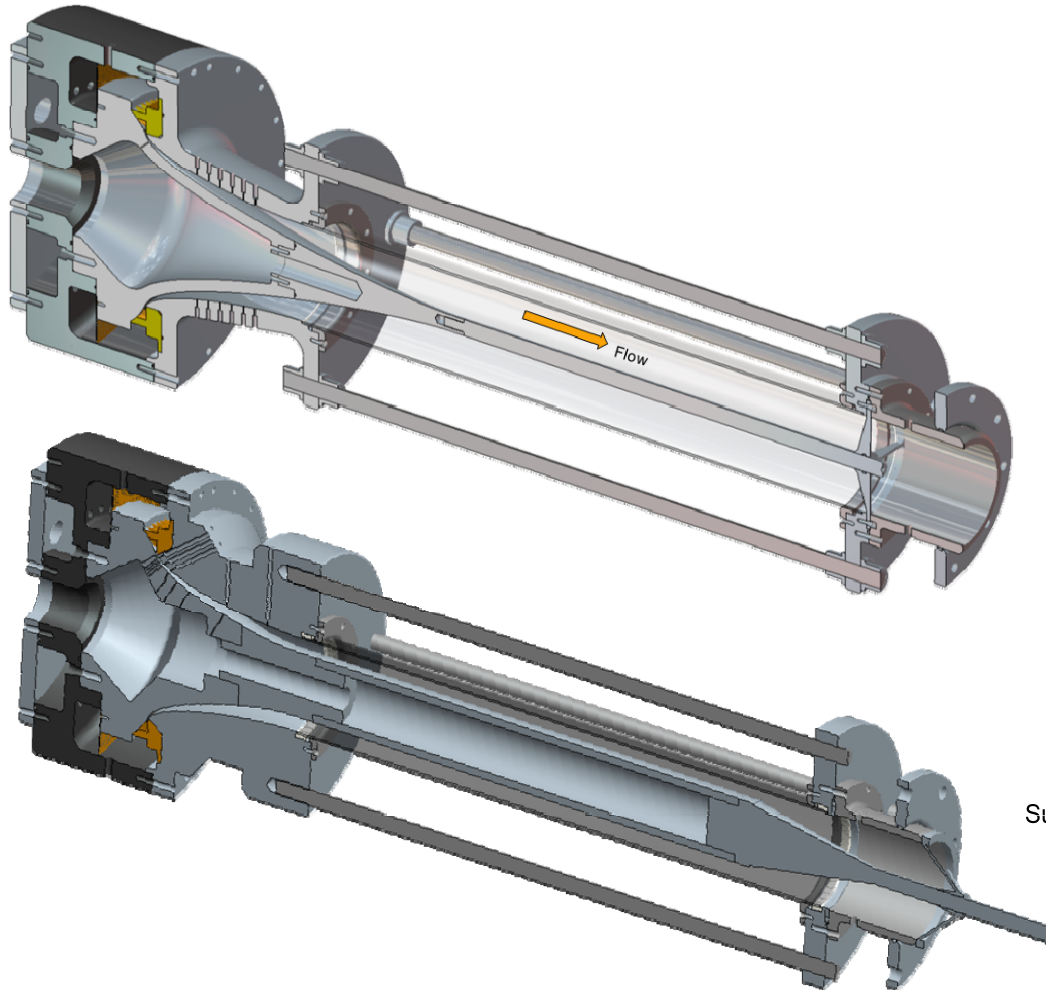
- Development of optimized supersonic contour to maximize particle size/migration and minimize pressure losses
- Minimization of “slip gas” that is removed with solid CO₂
- CO₂ purity unknowns - other flue gas impurities that condense will be removed with the CO₂
- Solid CO₂ management/self pressurization
- This really is rocket science....but once the design is complete, it is easy and inexpensive to build and operate

Project Status – Phase 1

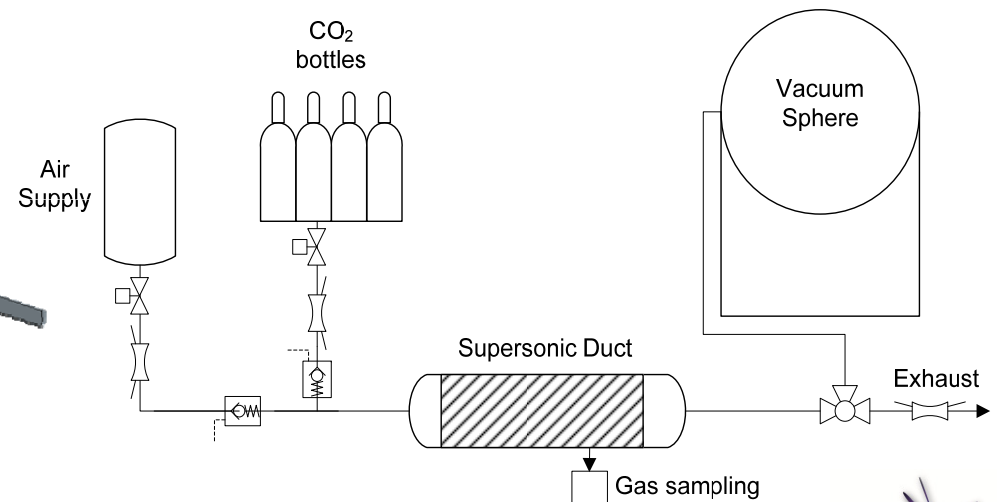


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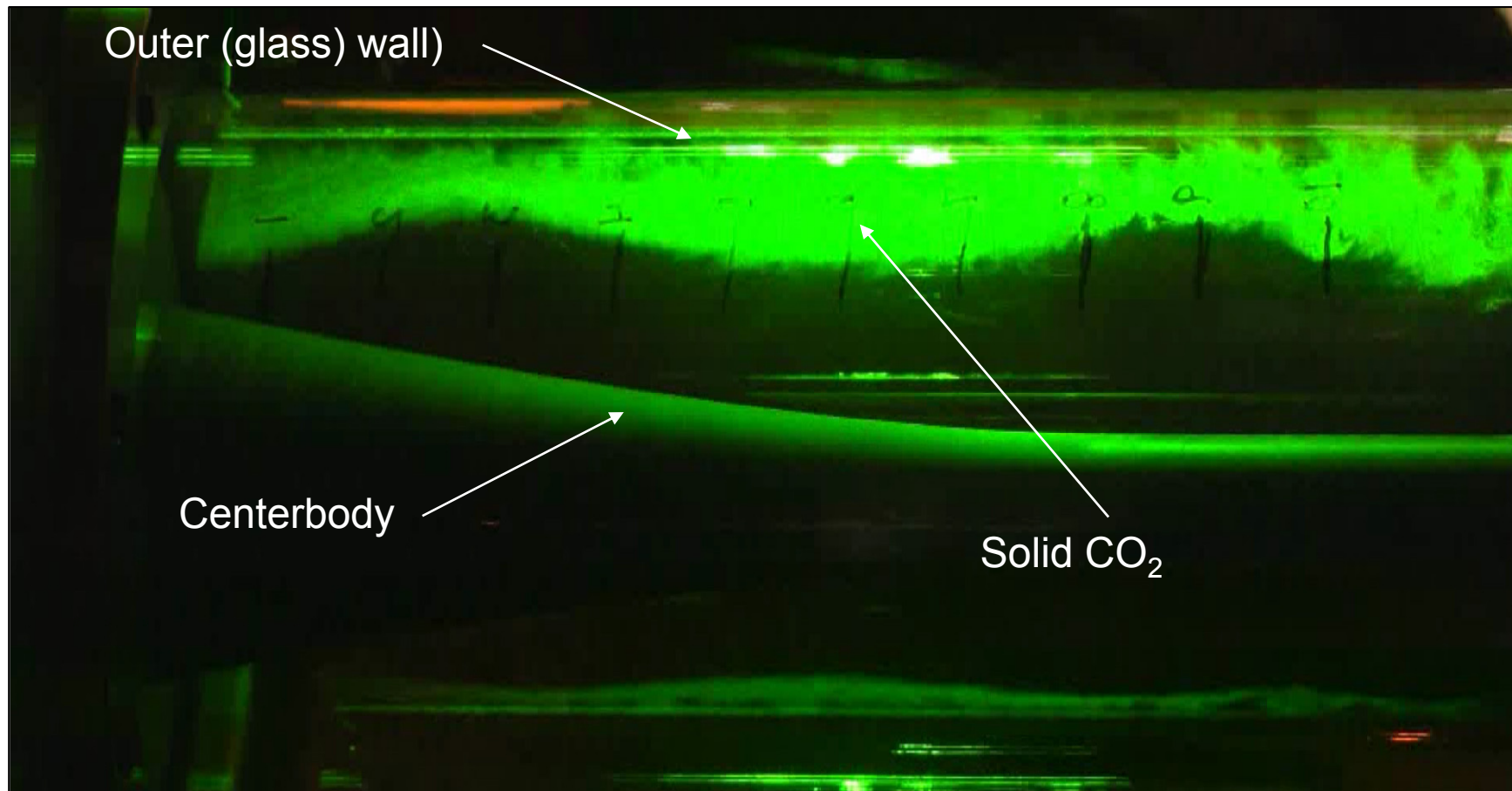
- Phase 1 and early Phase 2 efforts focused on an axisymmetric system with swirl



ICES test bench



Phase 1 data showed good CO₂ condensation and apparent, but erratic migration due to unsteady and separated flow

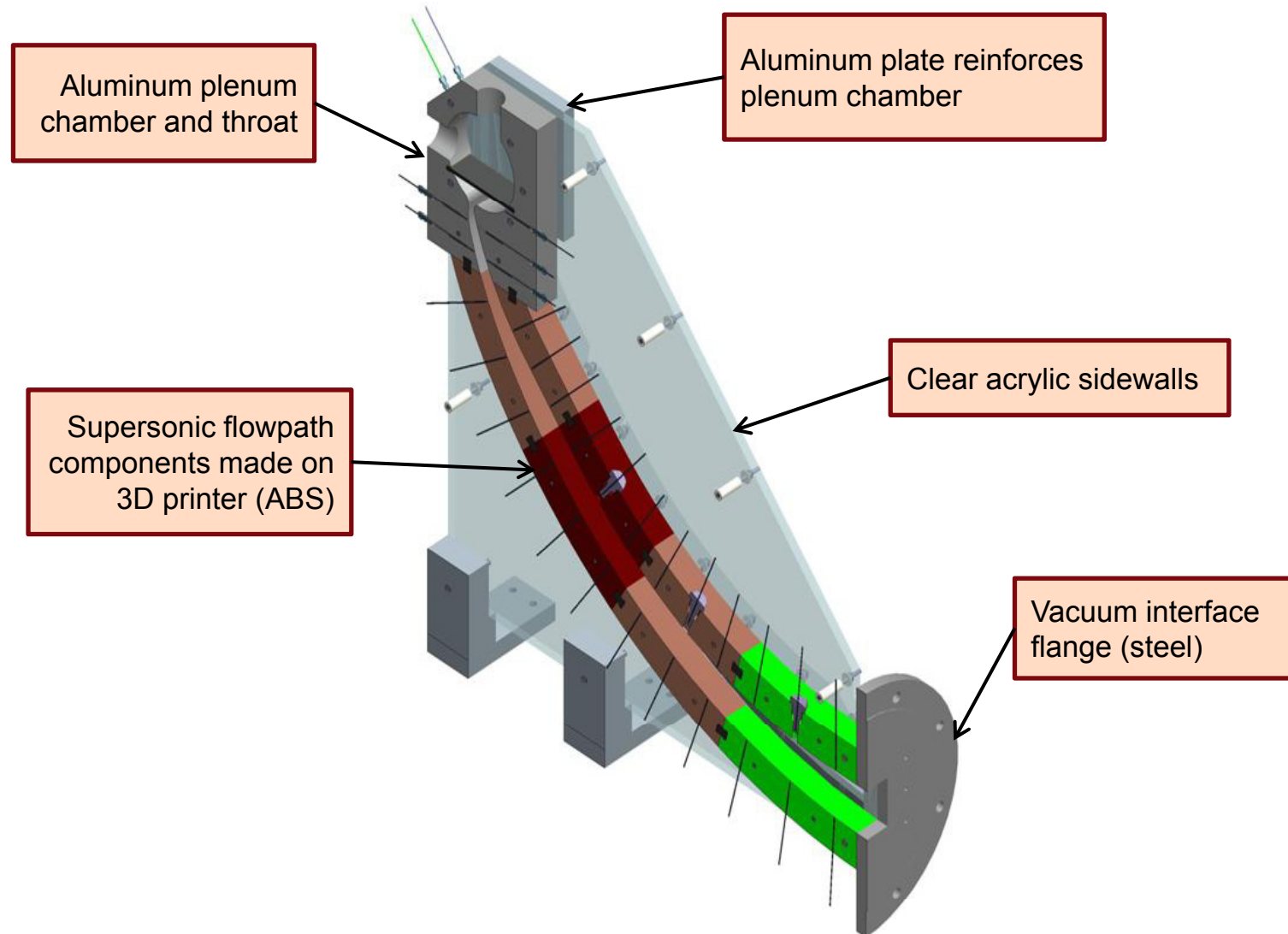


We recently changed to a 2D version of ICES



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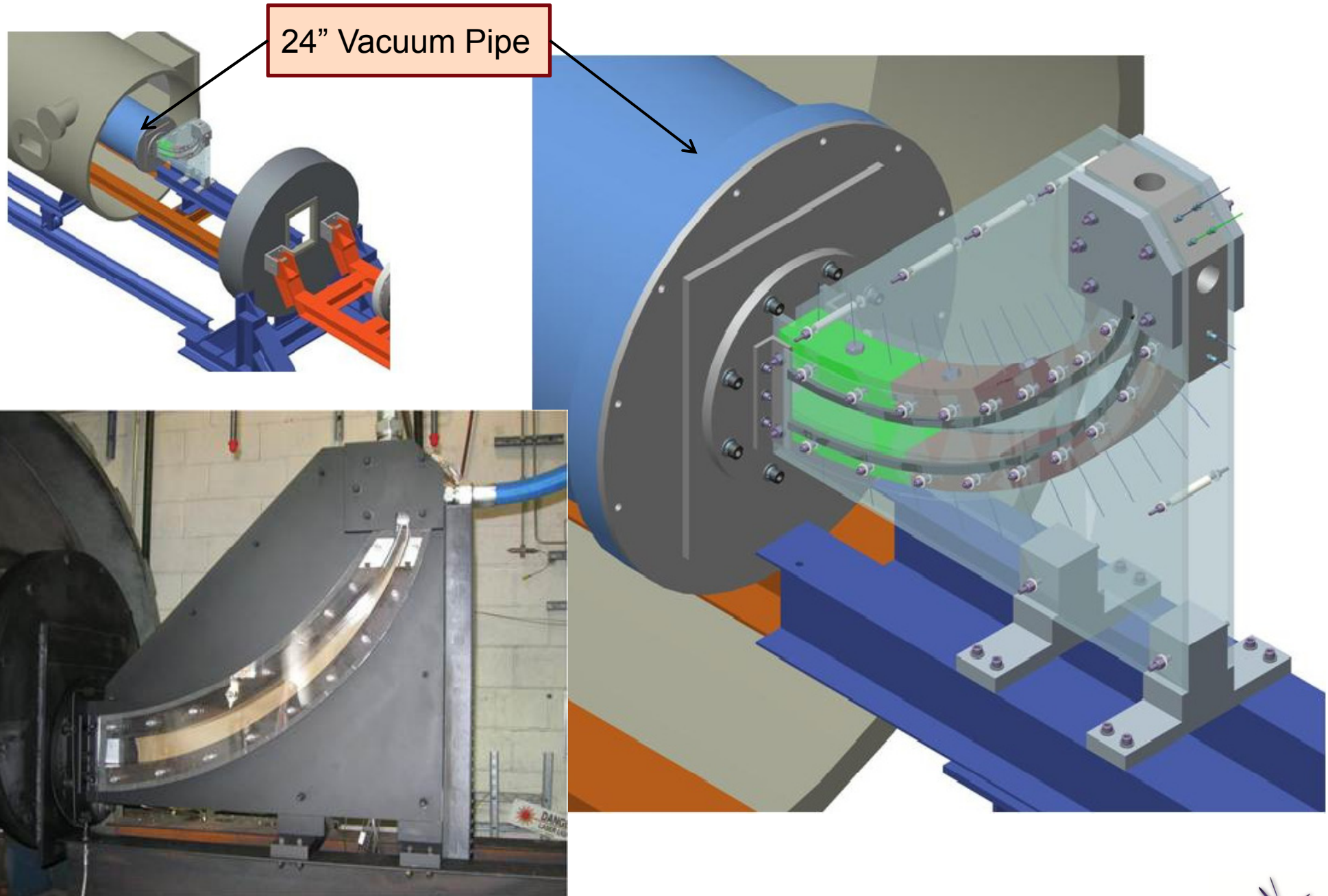
- Better aerodynamic performance (lower losses)
- Easier to fabricate and test
- No swirl vanes to induce turbulence/wake effects
- Simpler capture duct without swirl



Gen5 Test Article Design – ATK Installation



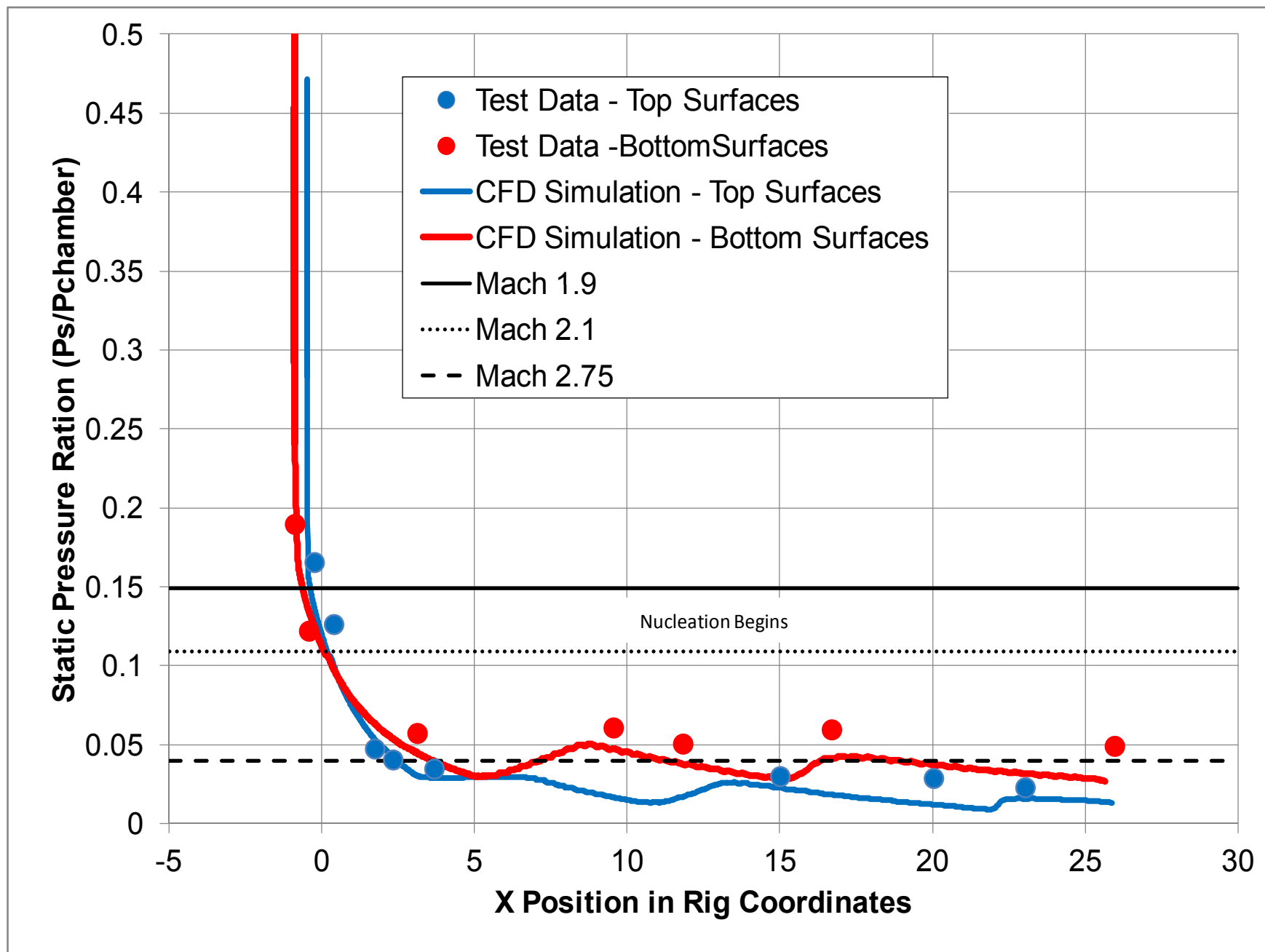
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Test Data Comparison to CFD – Static Pressure



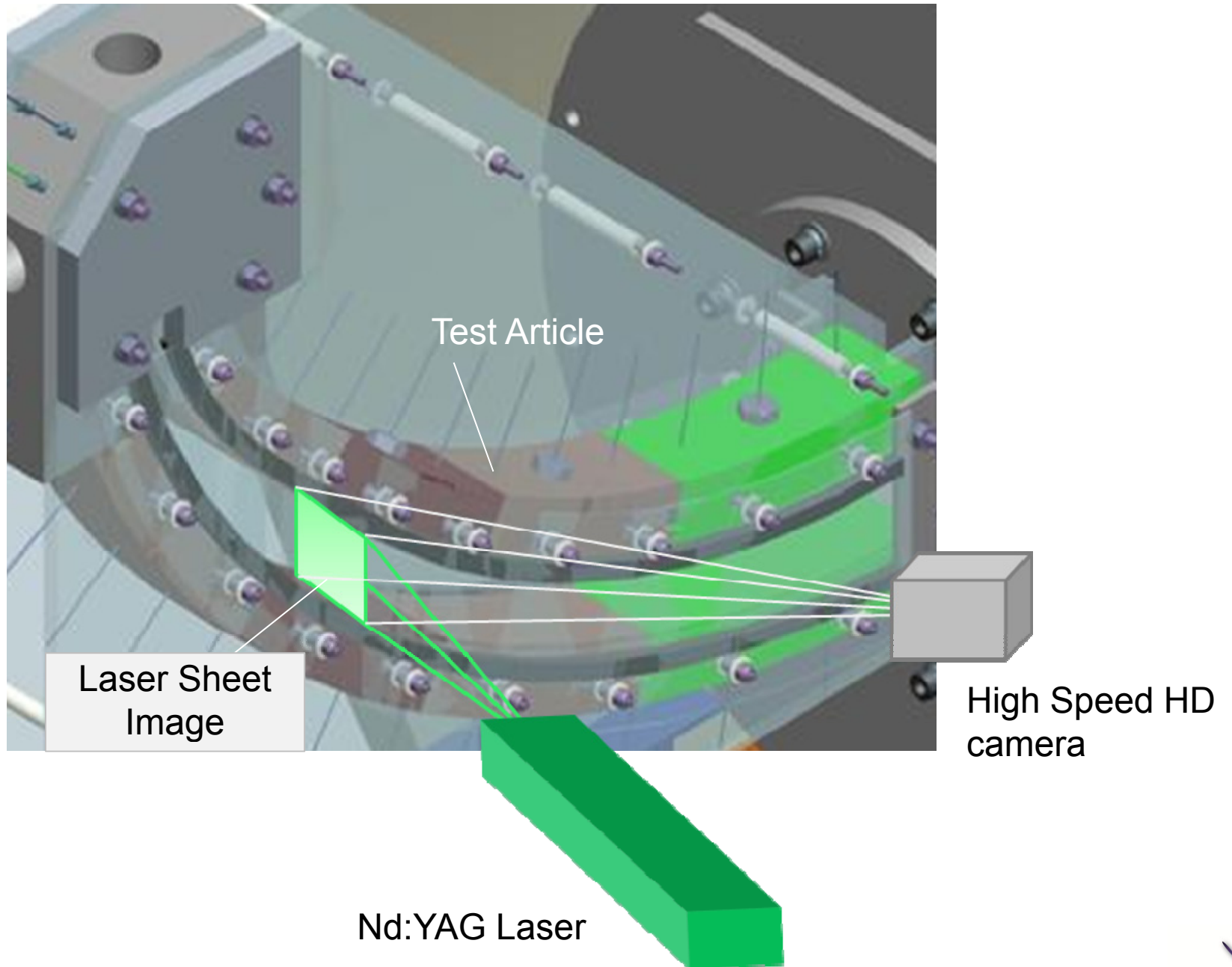
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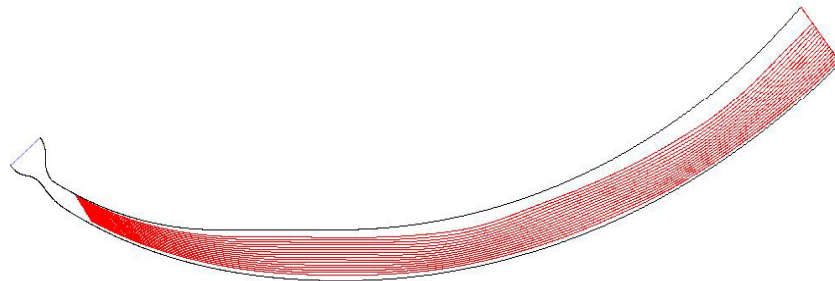
Laser Particle Imaging Diagnostic



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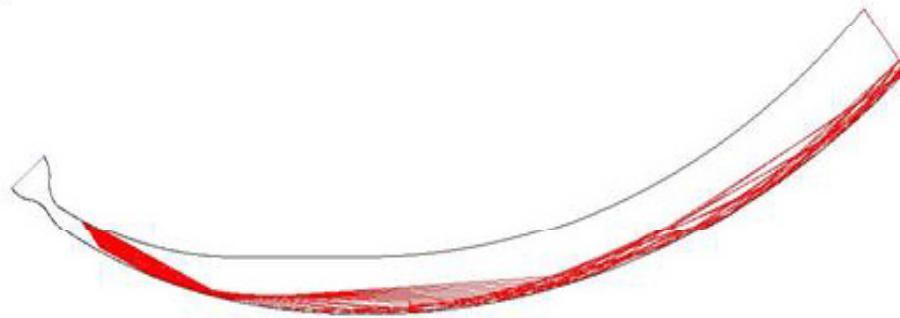


1, 10, and 100 Micron Particle Trajectories



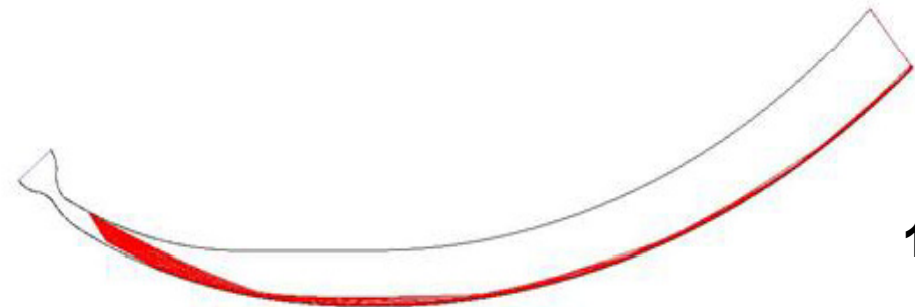
1 μm

1 Micron Particles - Released at Mach 2 Characteristic



10 μm

10 Micron Particles - Released at Mach 2 Characteristic

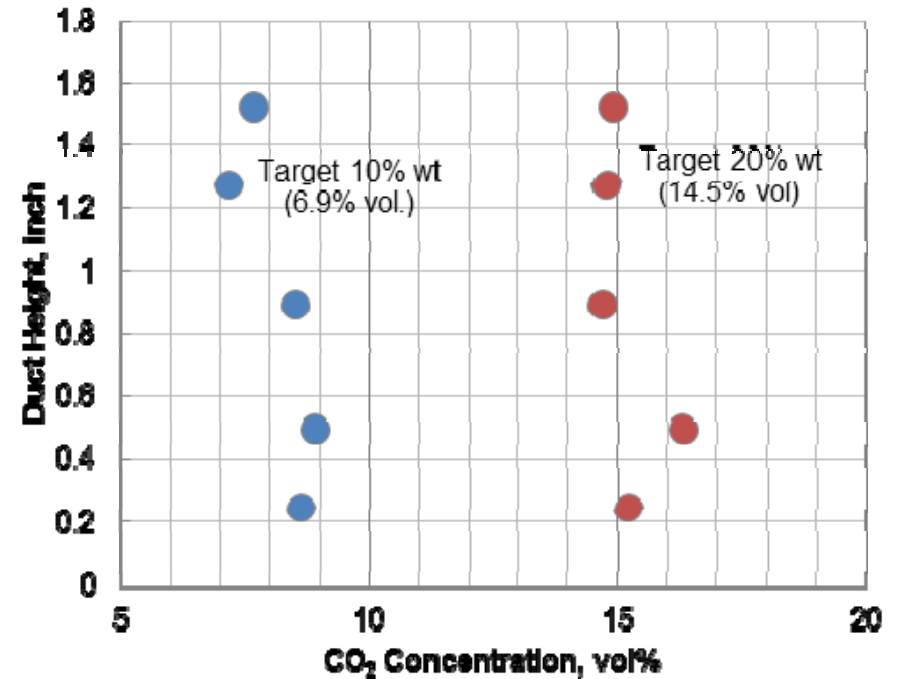
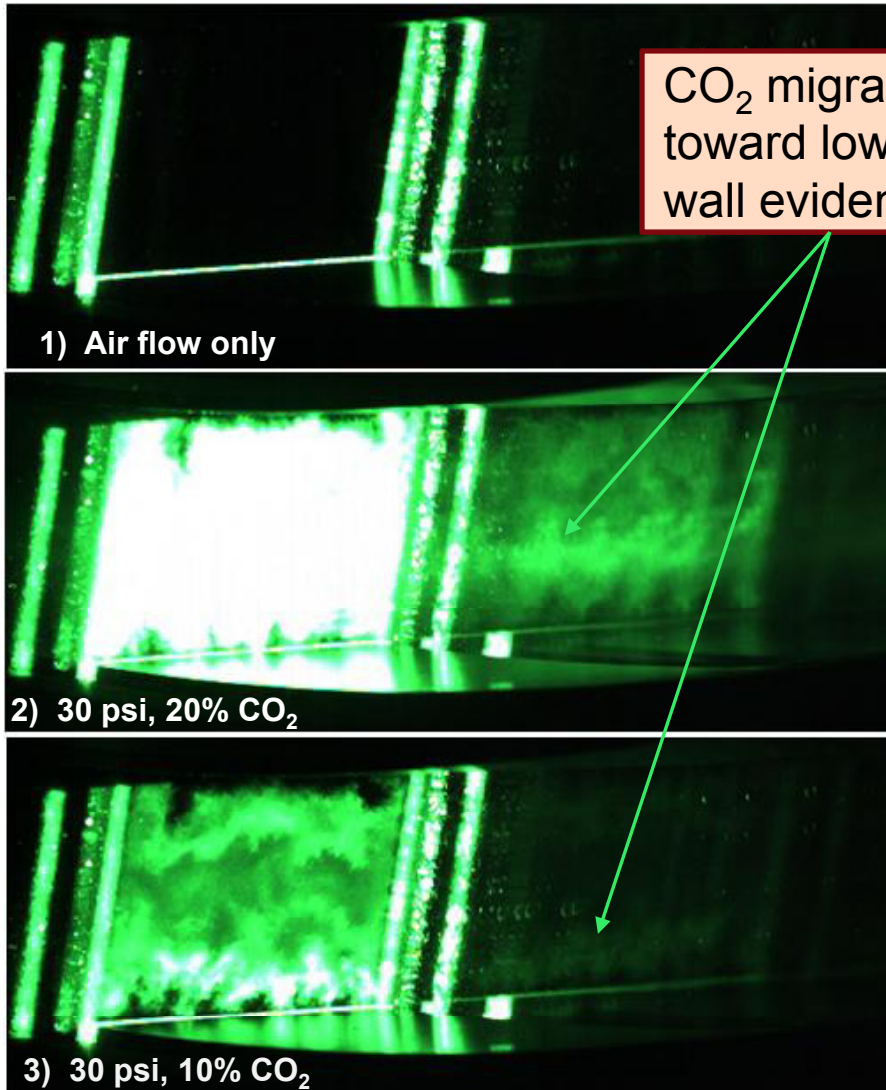


100 μm

100 Micron Particles - Released at Mach 2 Characteristic

At 10 microns+ particles separate and coalesce allowing for a slender capture slot

Three modes in typical ICES test

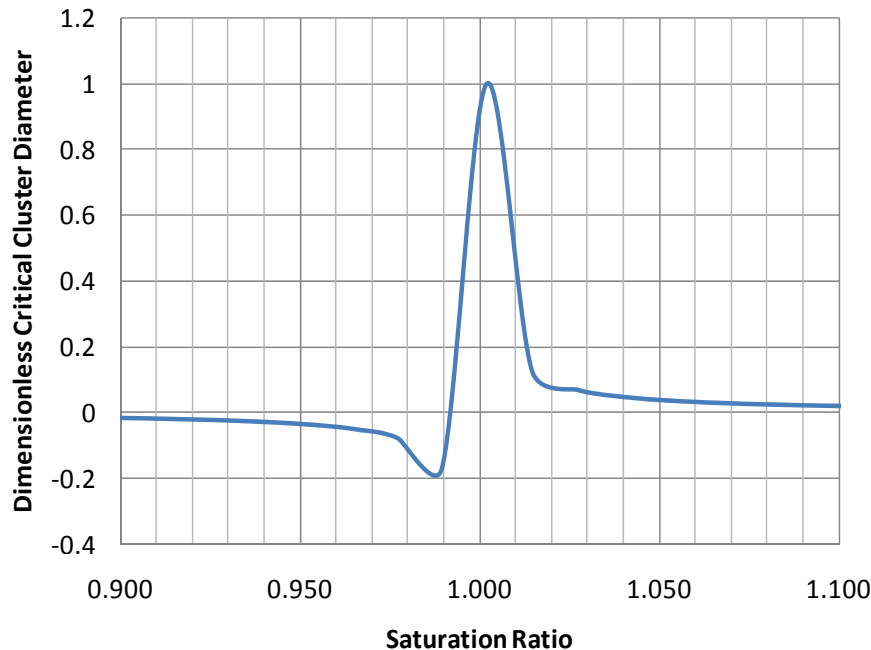


Optical and CO₂ sampling results show condensation as expected, but less than desired migration evident. Particle size does not appear large enough in these tests

- Classical nucleation theory provides basis for predicting critical condensate cluster size and subsequent growth rate:

$$r^* = \frac{2\sigma}{\rho_c RT \ln\left(\frac{p_v}{p_s}\right)} \quad \frac{dr}{dt} = \alpha \left[1 - \left(\frac{p_v}{p_s}\right)^{\left(\frac{r^*}{r} - 1\right)} \right] \left(\frac{m_c}{\rho_c}\right) \left[\frac{p_v}{(2\pi\bar{m}_c kT)^{1/2}}\right]$$

- Both are strong function of the saturation ratio (S) = partial pressure of vapor/saturation pressure (p_v/p_s)



- Maximum initial cluster size near S=1
- Desirable to grow these clusters versus nucleating new ones at higher S
- Nozzle contour shape needs to be optimized for this purpose
- Need to further increase residence time of flow in this critical region
- Increasing scale toward power plant size will help

- **Remaining portion of Phase 2**

- Investigate flow seeding with solid CO₂ (self generated) and other media to promote large particle formation (ongoing)
- Update contour to further optimize particle size
- Integration of capture duct to remove CO₂
- Integration of diffuser to return flow to atmospheric pressure with minimal losses

- **“Phase 3”**

- Ideal next step desired is a slip stream test, e.g. at the National Carbon Capture Center (NCCC)

- Three ICES configurations have been developed and tested to date
- Demonstrated clean nozzle flow with low apparent losses (to be verified with later diffuser tests)
- Demonstrated supersonic condensation with some migration
- Plans in place to increase particle size to achieve desired migration performance

ARPA E:

Dr. Karma Sawyer, Dr. Scott Litzelman, Dr. Daniel Matuszak, Dr. Mark Hartney

NYSERDA:

Dr. Barry Liebowitz

ATK & ACENT Labs:

Dr. Pat Sforza, Troy Custodio, Vincenzo Verrelli, Skip Day, Dean Feola, Ed Mihalik, Florin Girlea, Kirk Featherstone, Fred Gregory, Randy Voland

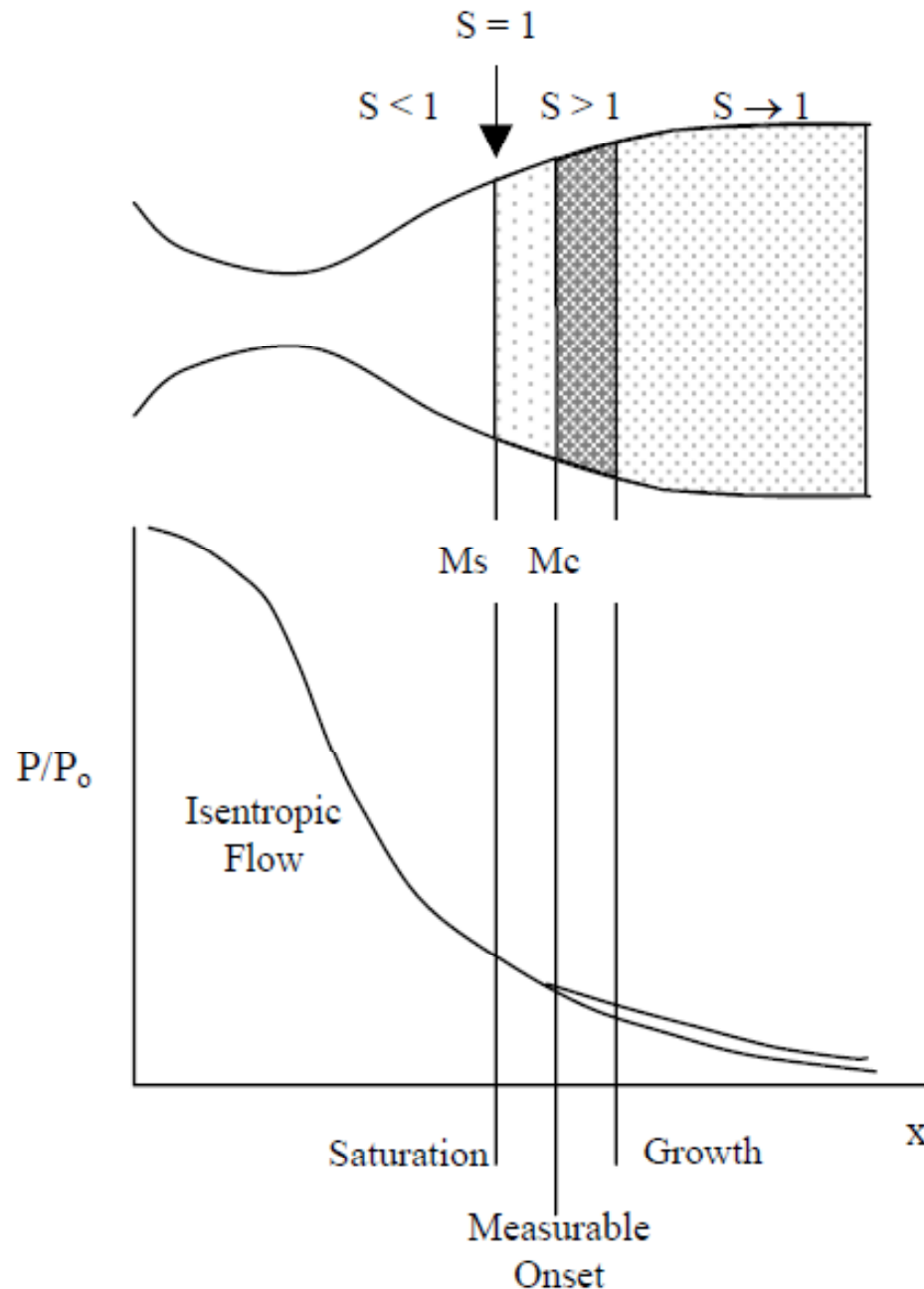




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BACKUP

Schematic of Condensation Process



$S = p_s / p_v$, where p_v is the partial pressure of the vapor and p_s is the vapor saturation pressure at the temperature of the system.